# **ORIGINAL PAPER**

Keyword



# InAs<sub>0.7</sub>Sb<sub>0.3</sub> Bulk Photodiodes Operating at Thermoelectric-Cooler Temperatures

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5 Current-voltage and photoelectrical characteristics of InAs<sub>0.7</sub>Sb<sub>0.3</sub> photo-

6 diodes grown onto InAs substrates are investigated in the interval of

7 212-330 K, i.e., the "thermoelectrical temperature range." The impacts of

8 mesa diameter, buffer layer thickness, and cooling on the zero-bias resistance

9 and spectral responsivity are described and analyzed. At low temperatures,

- 10 the dynamic zero-bias resistance dominat the serial one, resulting in the
- specific detectivity at 6.5  $\mu$ m and at T = 233 K being as high as
- 12  $3.2 \cdot 10^8 \text{ cm} \cdot \text{Hz}^{1/2} \cdot \text{W}^{-1}$  for a flat-plate photodiode.

# 13 1. Introduction

14 CdHgTe and InAsSb alloys have been traditionally used for many

15 years as "bulk" absorbing layers in barrier and conventional mid-IR photodiodes (PDs) that have found applications in gas 16 sensing,<sup>[1]</sup> IR thermometry,<sup>[2]</sup> and thermal imaging. Both alloys 17 have a specific band structure that, despite the misfit dislocations 18 formed during the growth on lattice mismatched substrates, 19 allows for p-n structures with a low dark current and high 20 quantum efficiency (see, e.g., Refs. [3-8]). For InAsSb-based 21 structures, the above property is believed to be enabled by their 22 23 unique property of producing electronic states above the conduction band, thereby suppressing the Shockley-Read-Hall 24 recombination processes.<sup>[9,10]</sup> There is thus a good chance for 25 manufacturing efficient PDs for radiation detection at wave-26 lengths exceeding 6 µm by using lattice mismatched substrates, 27 e.g., InAs substrates for the InAs<sub>1-x</sub>Sb<sub>x</sub>/InAs (x > 0.2,  $\Delta a$ / 28 29 a > 0.015) heterostructure PDs. In certain cases, the InAs<sub>1-x</sub>Sb<sub>x</sub>/InAs structures are beneficial with respect to 30  $InAs_{1-x}Sb_x/GaSb$  structures because the former offer narrow 31 bandwidth when illuminated from a side of the InAs substrate 32 that cuts off radiation with wavelengths shorter than  $\approx 3 \,\mu m$ . 33

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buffer layer thickness, and cooling on the 12 zero-bias resistance and spectral respon- 13 sivity values mainly in the temperature 14

This makes InAs-based PDs "blind" to 1

high-power medical lasers operating in the  $2 \mu m$  range and thus allows simultaneous 3

efficient delivery of high power through a 4

fiber and precise detection of thermal 5

radiation intensity and temperature meas- 6

urements of the fiber tip performed in the 7

In this paper, we study InAs<sub>0.7</sub>Sb<sub>0.3</sub> PDs 9

grown onto InAs substrates, with an 10

emphasis on an impact of mesa diameter, 11

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range of 212–330 K, usually referred to as the "thermoelectrical 15 temperature range." 16

 $3-5 \,\mu m$  spectral range.

# 2. Experimental Methods and Sample Description

Shown in Figure 1 are the chemical composition, interpolated 19 energy gap  $E_{g}^{300 \text{ K}}(X,Y)$ , and lattice constant mismatch (8*a*/*a*) of 20 the InAs<sub>1-x-y</sub>Sb<sub>x</sub>P<sub>y</sub> alloy versus distance in a typical structure 21 grown onto InAs substrate using a liquid-phase epitaxy method. 22 The heterostructures with a  $4-9 \,\mu m$  thick n-InAsSb buffer layer, 23 a 3 µm thick n-InAsSb active layer, and a 3 µm thick 24 P-InAsSbP(Zn) contact layer were processed using standard 25 optical photolithography into rectangular flip-chip PDs. The PD 26 chips of design described elsewhere<sup>[11]</sup> include an  $\approx 100 \,\mu\text{m}$  27 thick n-InAs substrate, a circular broad metal anode on top of 28 35–250 µm wide circular active areas (mesas) with an unpassi-29 vated sidewall and a "horse shoe" metal cathode on the n-InAs 30 substrate. Usually, there is sufficient spatial redistribution of 31 radiation in flip-chip PDs<sup>[11]</sup>; thus, for the sake of the adequate 32 optical area/responsivity evaluation, some PDs chips were 33 additionally equipped with an opaque diaphragm with known 34 open area or a hyperhemispherical Si immersion lens ( $\emptyset$  = 35 3.5 mm) glued onto the InAs substrate via a layer of chalcogenide 36 glass with n = 2.4. 37

**Figure 2**(a) demonstrates room temperature (RT) hetero- 38 structure (wafer) transparency and electroluminescence (EL) and 39 negative luminescence (NL) spectra both peaked at the photon 40 energy of 180 meV, which is quite close to the  $InAs_{0.7}Sb_{0.3}$  41 interpolated energy gap. *L*–*I* characteristics for both NL and EL 42 operation modes (see Figure 2(b)) were almost linear, with a peak 43 power of 3  $\mu$ W at a forward current of I = 1 A (0.003 mW A<sup>-1</sup>) at 44 RT for the diode with the immersion lens. The latter value is 45





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**Figure 1.** Mole fraction of InSb (X,  $\bigtriangledown$ ), InP (Y,  $\bigcirc$ ) and simulated energy gap  $E_{g}(X, Y)$  (**a**) and lattice mismatch with the InAs substrate ( $\Delta a/a$ , **a**) at room temperature versus distance in InAsSb<sub>0.3</sub> PD.

close to the power of the uncoated InAsSb<sub>0.44</sub> "barrier LEDs"
 with similar spectral characteristics when cooled down to 77 K in
 Ref. [12].

#### 4 3. Results and Discussion

Figure 3 shows the "raw data" zero-bias resistance-area product 5  $(R_0A = A \times dU/dI)$  at RT as a function of mesa diameter  $D_m$ . As 6 seen from the data in Figure 3, the  $R_0A$  product progressively 7 decreases and conductivity increases as the PD lateral 8 dimensions approach zero, indicating the presence of both 9 10 bulk and surface leakage currents. The leakage current density was evaluated in a manner similar to that presented in Ref. [13], 11 that is, from the dependence of a total dark current on mesa 12 diameter. The corresponding data together with best fit curves 13 presenting the simulated bulk  $I_{p-n}$ , the surface leakage  $I_{surf.}$ , and 14 15 the total ( $I_{p-n} + I_{surf}$ ) currents at U = -0.1 V and U = -0.2 V are 16 shown in Figure 4. As seen from Figure 4, the surface leakage 17 current ( $J_{\rm surf.} = 0.1 \, {\rm A \, cm^{-1}}$  at  $U = -0.1 \, {\rm V}$ ) dominates the bulk 18 one starting at mesa diameter less than  $\approx 17 \,\mu m$ .



**Figure 2.** Room temperature EL and NL spectra together with the p-n structure transmission (a) and the *L*-*I* characteristic of the immersion lens PDs (b).



Figure 3. "Raw data" zero-bias resistance-area product ( $R_oA$ ) versus mesa diameter  $D_m$ .

In general, an RT serial resistance  $R_s$  in narrow gap structures 1 of a large lateral size is usually much greater than the dynamic 2 p-n junction resistance, resulting in a nearly linear I-V 3 characteristic for most forward-bias voltages Uforw. (see, e.g., 4 Ref. [14]). In such cases the I-V characteristic relative solely to 5 the p-n junction properties could be obtained by extracting the 6 voltage drop across the serial resistance in the following manner: 7  $U_{p-n} = U_{forw} - R_s I$ , where  $U_{p-n}$  is understood as a voltage across 8 the p–n junction, and  $R_{\rm s} = dU_{\rm forw}/dI$  at  $U_{\rm forw} > 0.1$  V. Shown in 9 Figure 5 are the  $I-V_{p-n}$  characteristics of the p-n junction in a 10 195  $\mu$ m wide PD with  $R_{\rm s} \approx 1 \Omega$  measured at several temper-11 atures achievable by a 2-stage thermoelectric cooling. As shown 12 in Figure 5, the  $I-V_{p-n}$  characteristics at 212, 233, 256, 273, and 13 295 K adequately meet the modified Shockley formula 14  $I = I_0 \cdot [\exp(eU_{p-n}/\beta kT) \cdot 1]$ , where e is the elementary charge,  $\beta$ 15 is the ideality factor, k is the Boltzmann constant, and T is the 16 temperature. The ideality factor  $\beta$  ranged from unity at T = 295 K 17

296 K 10 Dark Current (A) 10 +/ 10 l surf InAsSb<sub>0.3</sub> PD #1146.8 10 6 8 10 20 40 60 80100 200 Mesa Diameter (um)

**Figure 4.** Total diode dark current at U = -0.1 ( $\blacksquare$ ) and -0.2 V ( $\Box$ ) (b) in InAsSb<sub>0.3</sub> PDs at room temperature. The lines present the simulated bulk  $(I_{p-n} = J_{p-n} \times \pi \times (D_m/2)^2, J_{p-n} = 56 \text{ A cm}^{-2})$  and surface leakage  $(I_{surf.} = J_{surf.} \times \pi \times D_m, J_{surf.} = 0.1 \text{ A cm}^{-1})$  currents as well the sum of the above two currents  $(I_{p-n} + I_{surf.})$  at U = -0.1 V.



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**Figure 5.** Dark current in InAsSb<sub>0.3</sub> PDs with an 8.8  $\mu$ m thick buffer layer versus bias applied to the p–n junction  $U_{p-n}$  at 212, 233, 256, 273, and 295 K. Solid lines represent the modified Shockley function.

1 to 3 at T = 212 K, indicating the dominance of the diffusion 2 current near RT and probably the dominance tunneling at 212 K, 3 respectively.

The prevalence of the diffusion current over other current 4 types near RT is also supported by an analysis of the temperature 5 dependence of the p-n junction zero-bias resistance-area 6 product defined as  $R_{p-n}A = \beta kTA/eI_o$ , where *e* is the electron 7 8 charge, and I<sub>o</sub> is the "saturation current" parameter derived from 9 the best fit of the above Shockley formula and experimental data in Figure 5. Indeed, the activation energy of an exponential 10 11 growth of the  $R_{p-n}A$  value near RT ( $E_a = 234$  meV, see the 12 Arrhenius plot in Figure 6) was close enough to the expected 13 energy gap value  $E_g(x,y) = 175 \text{ meV}$  (see data presented in Figure 1). The  $R_{p-n}A$  values at T = 250-300 K appeared higher 14 than RoA published by Razeghi<sup>[3]</sup> for the InAsSb/InSb 15 heterostructure PDs with nearly similar spectral response; in 16



**Figure 6.** Zero-bias resistance–area product of the p–n junction  $(R_{p-n}A, \blacksquare)$ and serial resistance–area product  $(R_sA, \Box)$  versus reciprocal temperature for a 195 µm wide mesa PD with an 8.8 µm thick buffer layer (all at the left scale) and temperature dependence of the term  $J_{dark}/T^3$  at a reverse bias of -0.1V ( $\blacklozenge$ ) and -0.4V ( $\bigtriangledown$ ) (both using the right scale). Solid lines denote the exp $(E_a/kT)$  and exp $(-E_a/kT)$  functions.



addition, at RT, the  $R_{p-n}A$  value is not far from the expectations 1 based on simulations made by Wróbel in Ref. [15]. 2

When comparing  $InAs_{0.7}Sb_{0.3}$  PDs with other detector types, 3 note that in some cases, the  $R_0A$  or  $R_{p-n}A$  value does not provide 4 adequate performance characterization. For example, barrier 5 detector current responsivity at small bias usually approaches 6 zero; as a result, normally, the figure of merit is the dark current 7 at a curtain bias and not the value of  $R_0A$ . The 233 K dark current 8 value  $J_{\text{dark}}$  in our PDs was several times smaller than that in 9 InAsSb<sub>0.4</sub> barrier photodiodes at U = -0.45 V with similar 10 spectral response<sup>[8,9]</sup> and was  $\approx 10$  times higher than the values 11 derived from the "Rule 07" directives.<sup>[16]</sup> Shown in Figure 6 is the 12 temperature dependence of the  $J_{\text{dark}}/T^3$  ratio at biases of -0.1 13 and -0.4 V, where the term  $T^3$  accounts for the temperature 14 dependence of the density of states in the expression for the 15 diffusion current density.<sup>[8]</sup> The activation energy of the  $J_{\text{dark}}/T^3$  16 exponential dependence at U = -0.1 V and T > 230 K was close 17 to that of the  $R_{p-n}A$ , that is, it was approximately two times higher 18 than that expected for a PD with dominant generation- 19 recombination current. 20

It is generally anticipated that the dark current in lattice- 21 mismatched PD structures declines with increasing buffer layer 22 thickness (see, e.g., Refs. [17,18]). In our case, however, the above 23 "rule of thumb" was not very well pronounced, as only minor PD 24 zero-bias resistance and sensitivity enhancement in PDs with 25 thick buffer could be traced from the data in Figure 7(b) and (c). 26 In contrast, a remarkable change in spectral response was 27 observed: the relative responsivity at short waves progressively 28 increased as the buffer layer thickness (t) decreased via the 29 collection efficiency enhancement in "thin buffer" structures, 30 e.g., from 0.3 at  $t=9\,\mu\text{m}$  up to 0.8 at  $t=4\,\mu\text{m}$  ( $\lambda=5\,\mu\text{m}$ ) (see 31 Figure 7(a)). The responsivity dependence on *t* suggests that the 32 hole diffusion length  $L_{\rm p}$  and a distance between the InAs/ 33 InAsSb and the p–n junctions are of the same order. Draft 34 evaluation provides values of  $L_p^{300 \text{ K}} \approx 6 \,\mu\text{m}$ , which are close to 35 the estimations of the same parameter in n-InAsSb-based PDs 36 given in Refs. [8,19,20] and approximately two times larger than 37 that in Ref. [6]. 38

The shortwave responsivity shoulder is obviously related to 39 the n-InAs substrate transparency spectrum; the longwave 40



**Figure 7.** Room temperature normalized photoresponse spectra (a), peak sensitivity (b), and dark current at -0.2 V (c) versus buffer layer thickness (*t*) in InAsSb<sub>0.3</sub> PDs.





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233 K Current sensitivity S, (A / W ) 253 K 273 K 296 K<sup>.</sup> 0.1 313 K 330 K InAsSb<sub>0.3</sub> F #1146.6 PD 0.01 3 4 5 6 8 9 7 Wavelength (µm)

Figure 8. Photoresponse spectra of the PD with  $3.9 \,\mu m$  thick buffer layer in the 233-330 K interval.

1 shoulder was temperature-sensitive with a 0.28 meV K<sup>-1</sup> 2 temperature shift rate close to InAs energy-gap variation (see Figure 8). The responsivity near the peak wavelength exhibited 3 nice growth upon cooling of the PD, as shown in Figure 8 and 9; 4 this result most likely highlights the prevalence of the p-n 5 junction resistance over  $R_s$  at low temperatures. At 233 K, the 6 195  $\mu$ m wide mesa PD zero-bias resistance-area product  $R_{o}A$  and 7 responsivity  $S_{\rm I}$  at a wavelength of 6.5 µm were 0.0015  $\Omega$  cm<sup>2</sup> 8 and  $1 \,\mathrm{AW}^{-1}$ , respectively, which are higher than those in 9 "commercial" CdHgTe detectors mounted onto a 2-stage 10 thermoelectric cooler (see, e.g., Ref. [21]). Coherently, the 11 simulated Johnson noise limited specific detectivity is also 12 13 higher than that in Ref. [21] (see Figure 9) and at  $\lambda = 6.5 \,\mu m$ 14 amounts to  $3.2 \cdot 10^8 \text{ cm} \cdot \text{Hz}^{1/2} \cdot \text{W}^{-1}$  for a bare chip PD. 15 Incorporation of a hyperhemispherical immersion Si lens 16 (Ø = 3.5 mm) increases the  $D_{6.5 \,\mu\text{m}, 233 \text{ K}}^*$  up to  $4.3 \cdot 10^9 \text{ cm} \cdot$ 



**Figure 9.** Specific detectivity  $D^*$  for bare chip (...) and immersion lens (.) PDs (left scale) and responsivity (right scale, **(**) at maximum versus temperature in a 195  $\mu$ m wide bare chip InAsSb<sub>0.3</sub> PD with 5  $\mu$ m thick buffer layer.

 $Hz^{1/2} \cdot W^{-1}$ , making InAsSb<sub>0.3</sub> PDs superior to the commercial 1 PDs, at least at wavelengths of  $\approx 6.5 \,\mu m$ . 2

#### 4. Conclusions

InAsSbP/InAsSb<sub>0.3</sub> p-n heterostructures grown onto InAs 4 substrates demonstrated diffusion-limited current at near room 5 temperature and tunnel current at 212-250 K with predomi-6 nantly series resistance in the temperature range of 270-300 K. 7 The zero-bias p-n junction resistance-area product was close to 8 the theoretical estimations, and the specific detectivity at 233 K 9 achievable by a 2-stage thermoelectric cooler amounted to 10 remarkable values of  $D_{6.5 \,\mu m}^* = 3.2 \cdot 10^8$  and  $4.3 \cdot 10^9$  Jones for 11 the 195  $\mu$ m wide bare chip and immersion lens PDs (Ø = 12 3.5 mm), respectively. 13

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# **Conflict of Interest**

The<sup>Q3</sup> authors declare no conflict of interest.

### Keywords

backside illuminated photodiodes, dark current, InAsSb photodiodes, infrared sensors, IR gas sensors, mid-IR detectors, pyrometry

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Low energy gap flip-chip photodiodes with InAsSb<sub>0.3</sub> absorbing layer have been fabricated. These photodiodes exhibit reasonably high values of specific detectivity and responsivity at 6.5  $\mu$ m when cooled down to 233 K which is essential for many spectroscopic measurements including pyrometry and gas analysis.

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